On the non-stabilizability for networks of strings

Martin Gugat, Friedrich-Alexander-Universität Erlangen-Nürnberg (FAU) joint work with Stephan Gerster (RWTH Aachen), see On the limits of stabilizability for networks of strings, Systems and Control Lett. 131 (2019) Control and stabilization of hyperbolic systems Benasque, Wednesday, August 28, 2019



Inhalt

Motivation by application: Gas transportation through pipelines Example for a closed-loop system.

The example by BASTIN and CORON: A single interval A sufficient condition for non-stabilzability A sufficient condition for stabilizability

A tree of strings with a stabilizing and a destabilizing source term Sufficient conditions for non-stabilzability A sufficient condition for stabilizability

Application: Gas transportation through pipelines

The system dynamics in a pipe is described by

the isothermal Euler equations

$$\begin{cases} \rho_t + q_x = \mathbf{0} \\ q_t + \left(\mathbf{p} + \frac{q^2}{\rho}\right)_x = -\frac{f_g}{2\delta} \frac{q|q|}{\rho} - \rho \, \mathbf{g} \, \sin(\alpha) \end{cases}$$

or a similar (linearized) model, see *A. Osiadacz, M. Chazykowski*, Comparison of isothermal and non-isothermal pipeline gas flow models, 2001.



See the results of DFG CRC 154:



Mathematical Modelling, Simulation and Optimization Using the Example of Gas Networks

Model for the flow in a single pipe

Ideal gas

In ideal gas, we have

$$p = c^2 \rho$$

The sound speed *c* is constant!

The isothermal Euler equations $\begin{cases} \rho_t + q_x = 0 \\ q_t + \left(p + \frac{q^2}{\rho}\right)_x = -\frac{f_g}{2\delta} \frac{q|q|}{\rho} \end{cases}$

In terms of the RIEMANN invariants the hyperbolic system has the quasilinear form

In terms of the RIEMANN invariants the hyperbolic system has the quasilinear form

 $R_t + D_q(R) R_x = F(R)$

with a diagonal matrix $D_q(R)$ that contains the eigenvalues

$$\frac{\boldsymbol{q}}{\rho} + \boldsymbol{c}, \ \ \frac{\boldsymbol{q}}{\rho} - \boldsymbol{c}$$

In terms of the RIEMANN invariants the hyperbolic system has the quasilinear form

 $R_t + D_q(R) R_x = F(R)$

with a diagonal matrix $D_q(R)$ that contains the eigenvalues

$$rac{m{q}}{
ho}+m{c}, \;\; rac{m{q}}{
ho}-m{c}$$

If we replace the eigenvalues by

$$d_+ = c, \ d_- = -c$$

we get a *semilinear* model with a constant matrix *D*.

In terms of the RIEMANN invariants the hyperbolic system has the quasilinear form

 $R_t + D_q(R) R_x = F(R)$

with a diagonal matrix $D_q(R)$ that contains the eigenvalues

$$rac{m{q}}{
ho}+m{c}, \;\; rac{m{q}}{
ho}-m{c}$$

If we replace the eigenvalues by

$$d_+ = c, \ d_- = -c$$

we get a *semilinear* model with a constant matrix D. Let a stationary state \overline{R} with $D\overline{R}_x = F(\overline{R})$ be given.

In terms of the RIEMANN invariants the hyperbolic system has the quasilinear form

 $R_t + D_q(R) R_x = F(R)$

with a diagonal matrix $D_q(R)$ that contains the eigenvalues

$$rac{m{q}}{
ho}+m{c}, \ \ rac{m{q}}{
ho}-m{c}$$

If we replace the eigenvalues by

$$d_+ = c, d_- = -c$$

we get a *semilinear* model with a constant matrix *D*. Let a stationary state \overline{R} with $D\overline{R}_x = F(\overline{R})$ be given. Linearizing around \overline{R} with $r = R - \overline{R}$ yields

 $r_t + Dr_x = F'(\bar{R})r.$

In terms of the RIEMANN invariants the hyperbolic system has the quasilinear form

 $R_t + D_q(R) R_x = F(R)$

with a diagonal matrix $D_q(R)$ that contains the eigenvalues

$$rac{m{q}}{
ho}+m{c}, \ \ rac{m{q}}{
ho}-m{c}$$

If we replace the eigenvalues by

$$d_+ = c, d_- = -c$$

we get a *semilinear* model with a constant matrix *D*. Let a stationary state \overline{R} with $D\overline{R}_x = F(\overline{R})$ be given. Linearizing around \overline{R} with $r = R - \overline{R}$ yields

$$r_t + Dr_x = F'(\bar{R})r.$$

For the ideal gas we get $F'(\bar{R}) = -2 \frac{f_g}{\delta} |\bar{R}_+(x) - \bar{R}_-(x)| \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix}$.

In terms of the RIEMANN invariants the hyperbolic system has the quasilinear form

 $R_t + D_a(R) R_x = F(R)$

with a diagonal matrix $D_q(R)$ that contains the eigenvalues

$$rac{m{q}}{
ho}+m{c}, \ \ rac{m{q}}{
ho}-m{c}$$

If we replace the eigenvalues by

$$d_+ = c, d_- = -c$$

we get a *semilinear* model with a constant matrix D. Let a stationary state \overline{R} with $D\overline{R}_x = F(\overline{R})$ be given. Linearizing around \overline{R} with $r = R - \bar{R}$ yields

$$r_t + Dr_x = F'(\bar{R})r.$$

For the ideal gas we get $F'(\bar{R}) = -2 \frac{f_g}{\delta} |\bar{R}_+(x) - \bar{R}_-(x)| \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix}$.

linearize!)

The matrix $\begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix}$ is positive semidefinite. (First go to RIEMANN invariants, then

In terms of the RIEMANN invariants the hyperbolic system has the quasilinear form

 $R_t + D_q(R) R_x = F(R)$

with a diagonal matrix $D_q(R)$ that contains the eigenvalues

$$rac{m{q}}{
ho}+m{c}, \ \ rac{m{q}}{
ho}-m{c}$$

If we replace the eigenvalues by

$$d_+ = c, d_- = -c$$

we get a *semilinear* model with a constant matrix *D*. Let a stationary state \overline{R} with $D\overline{R}_x = F(\overline{R})$ be given. Linearizing around \overline{R} with $r = R - \overline{R}$ yields

$$r_t + Dr_x = F'(\bar{R})r.$$

For the ideal gas we get $F'(\bar{R}) = -2 \frac{f_g}{\delta} |\bar{R}_+(x) - \bar{R}_-(x)| \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix}$.

The matrix $\begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix}$ is positive semidefinite. (**First go to** RIEMANN **invariants, then linearize!**) The *pressure* is given by $\exp\left(\frac{1}{2}\left(r_{+} + r_{-} + \bar{R}_{+} + \bar{R}_{-}\right)\right) > 0$ and the gas *velocity* is proportional to $r_{+} - r_{-} + \bar{R}_{+} - \bar{R}_{-}$.

We are interested in **boundary control** of the system!

For this purpose, we introduce a control u(t) in the boundary condition.

We are interested in **boundary control** of the system!

For this purpose, we introduce a control u(t) in the boundary condition. For example DIRICHLET boundary control

 $r_+(t, 0) = u_+(t), r_-(t, L) = u_-(t).$

We are interested in **boundary control** of the system!

For this purpose, we introduce a control u(t) in the boundary condition. For example DIRICHLET boundary control

$$r_+(t, 0) = u_+(t), \ r_-(t, L) = u_-(t).$$

What happens if in the pde

$$r_t + Dr_x = -Mr$$

the matrix is *not* positive definite? Can this cause difficulties?

We are interested in **boundary control** of the system!

For this purpose, we introduce a control u(t) in the boundary condition. For example DIRICHLET boundary control

$$r_+(t, 0) = u_+(t), \ r_-(t, L) = u_-(t).$$

What happens if in the pde

$$r_t + Dr_x = -Mr$$

the matrix is *not* positive definite? Can this cause difficulties?

Yes!

Inhalt

Motivation by application: Gas transportation through pipelines Example for a closed-loop system.

The example by BASTIN and CORON: A single interval A sufficient condition for non-stabilzability A sufficient condition for stabilizability

A tree of strings with a stabilizing and a destabilizing source term Sufficient conditions for non-stabilzability A sufficient condition for stabilizability

Example for a closed-loop system.

 $\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

Together with the boundary conditions

$$U(t, 0) = k V(t, 0), V(t, L) = U(t, L)$$

where $k \in (-1, 1)$ is a **feedback parameter** (and initial data $U(0, \cdot), V(0, \cdot)$)) we have a **closed loop-system.**

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

Together with the boundary conditions

$$U(t, 0) = k V(t, 0), V(t, L) = U(t, L)$$

where $k \in (-1, 1)$ is a **feedback parameter** (and initial data $U(0, \cdot), V(0, \cdot)$)) we have a **closed loop-system.**

For k = 0 it is *finite time stable*.

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

Together with the boundary conditions

$$U(t, 0) = k V(t, 0), V(t, L) = U(t, L)$$

where $k \in (-1, 1)$ is a **feedback parameter** (and initial data $U(0, \cdot), V(0, \cdot)$)) we have a **closed loop-system.**

For k = 0 it is *finite time stable*.

In the applications, often **source terms** play an essential role.

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

Together with the boundary conditions

$$U(t, 0) = k V(t, 0), V(t, L) = U(t, L)$$

where $k \in (-1, 1)$ is a **feedback parameter** (and initial data $U(0, \cdot), V(0, \cdot)$)) we have a **closed loop-system.**

For k = 0 it is *finite time stable*.

In the applications, often **source terms** play an essential role.

In our example, with a 2×2 matrix *M* we get

$$\begin{pmatrix} U \\ V \end{pmatrix}_t + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_x + M \begin{pmatrix} U \\ V \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}.$$

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

Together with the boundary conditions

$$U(t, 0) = k V(t, 0), V(t, L) = U(t, L)$$

where $k \in (-1, 1)$ is a **feedback parameter** (and initial data $U(0, \cdot), V(0, \cdot)$)) we have a **closed loop-system.**

For k = 0 it is *finite time stable*.

In the applications, often **source terms** play an essential role.

In our example, with a 2×2 matrix *M* we get

$$\begin{pmatrix} U \\ V \end{pmatrix}_t + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_x + M \begin{pmatrix} U \\ V \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}.$$

The source term can cause instability!

Outline

Motivation by application: Gas transportation through pipelines Example for a closed-loop system.

The example by BASTIN and CORON: A single interval

A sufficient condition for non-stabilzability A sufficient condition for stabilizability

A tree of strings with a stabilizing and a destabilizing source term Sufficient conditions for non-stabilzability A sufficient condition for stabilizability

Inhalt

Motivation by application: Gas transportation through pipelines Example for a closed-loop system.

The example by BASTIN and CORON: A single interval

A sufficient condition for non-stabilzability A sufficient condition for stabilizability

A tree of strings with a stabilizing and a destabilizing source term Sufficient conditions for non-stabilzability A sufficient condition for stabilizability

In Stability and Boundary Stabilization of 1-D Hyperbolic Systems (2016), BASTIN and CORON consider the diagonal system

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} + \begin{pmatrix} 0 & c \\ c & 0 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

with a real parameter c > 0.

In Stability and Boundary Stabilization of 1-D Hyperbolic Systems (2016), BASTIN and CORON consider the diagonal system

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} + \begin{pmatrix} 0 & c \\ c & 0 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

with a real parameter c > 0.

Together with the boundary conditions

$$U(t, 0) = k V(t, 0), V(t, L) = U(t, L)$$

where $k \in (-1, 1)$ is a feedback parameter (and initial data $U(0, \cdot), V(0, \cdot)$)) we have a **closed loop-system**.

In Stability and Boundary Stabilization of 1-D Hyperbolic Systems (2016), BASTIN and CORON consider the diagonal system

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} + \begin{pmatrix} 0 & c \\ c & 0 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

with a real parameter c > 0.

Together with the boundary conditions

$$U(t, 0) = k V(t, 0), V(t, L) = U(t, L)$$

where $k \in (-1, 1)$ is a feedback parameter (and initial data $U(0, \cdot), V(0, \cdot)$)) we have a **closed loop-system**.

Is it stable?

In Stability and Boundary Stabilization of 1-D Hyperbolic Systems (2016), BASTIN and CORON consider the diagonal system

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} + \begin{pmatrix} 0 & c \\ c & 0 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

with a real parameter c > 0.

Together with the boundary conditions

$$U(t, 0) = k V(t, 0), \quad V(t, L) = U(t, L)$$

where $k \in (-1, 1)$ is a feedback parameter (and initial data $U(0, \cdot), V(0, \cdot)$)) we have a **closed loop-system**.

Is it stable?

BASTIN & CORON construct product solutions of the form (separation ansatz)

$$\begin{pmatrix} U(t, x) \\ V(t, x) \end{pmatrix} = \exp(\sigma t) \begin{pmatrix} f(x) \\ g(x) \end{pmatrix}$$

If such a solution can be found with $\sigma > 0$, the system is *exponentially unstable* and cannot be stabilized.

For $\sigma \in (0, c)$ define $\omega = \sqrt{c^2 - \sigma^2} > 0$. The pde and f(0) = k g(0) imply

$$f(x) = (c + k\sigma) \sin(\omega x) - k \omega \cos(\omega x),$$

$$g(x) = -(\sigma + kc) \sin(\omega x) - \omega \cos(\omega x).$$

For $\sigma \in (0, c)$ define $\omega = \sqrt{c^2 - \sigma^2} > 0$. The pde and f(0) = k g(0) imply

$$f(x) = (c + k\sigma) \sin(\omega x) - k \omega \cos(\omega x),$$

$$g(x) = -(\sigma + kc) \sin(\omega x) - \omega \cos(\omega x).$$

For $\sigma \in (0, c)$ define $\omega = \sqrt{c^2 - \sigma^2} > 0$. The pde and f(0) = k g(0) imply

$$f(x) = (c + k\sigma) \sin(\omega x) - k \omega \cos(\omega x),$$

$$g(x) = -(\sigma + kc) \sin(\omega x) - \omega \cos(\omega x).$$

For $k \neq -1$ we have f(L) = g(L) if $\sigma \in (0, c)$ is such that

$$(\sigma + \mathbf{C}) \frac{\tan(\sqrt{\mathbf{C}^2 - \sigma^2} L)}{\sqrt{\mathbf{C}^2 - \sigma^2}} = \frac{k-1}{k+1}.$$

For $\sigma \in (0, c)$ define $\omega = \sqrt{c^2 - \sigma^2} > 0$. The pde and f(0) = k g(0) imply

$$f(x) = (c + k\sigma) \sin(\omega x) - k \omega \cos(\omega x),$$

$$g(x) = -(\sigma + kc) \sin(\omega x) - \omega \cos(\omega x).$$

For $k \neq -1$ we have f(L) = g(L) if $\sigma \in (0, c)$ is such that

$$(\sigma + \mathbf{C}) \frac{\tan(\sqrt{\mathbf{C}^2 - \sigma^2} L)}{\sqrt{\mathbf{C}^2 - \sigma^2}} = \frac{k-1}{k+1}.$$

For k = -1 we have f(L) = g(L) if $\sigma \in (0, c)$ is such that

$$0=\cos(\sqrt{c^2-\sigma^2}\,L).$$

For $\sigma \in (0, c)$ define $\omega = \sqrt{c^2 - \sigma^2} > 0$. The pde and f(0) = k g(0) imply

$$f(x) = (c + k\sigma) \sin(\omega x) - k \omega \cos(\omega x),$$

$$g(x) = -(\sigma + kc) \sin(\omega x) - \omega \cos(\omega x).$$

For $k \neq -1$ we have f(L) = g(L) if $\sigma \in (0, c)$ is such that

$$(\sigma + \mathbf{C}) \frac{\tan(\sqrt{\mathbf{C}^2 - \sigma^2} L)}{\sqrt{\mathbf{C}^2 - \sigma^2}} = \frac{k-1}{k+1}.$$

For k = -1 we have f(L) = g(L) if $\sigma \in (0, c)$ is such that

$$\mathbf{0}=\cos(\sqrt{\mathbf{C}^2-\sigma^2}\,\mathbf{L}).$$

This is possible if *c L* is sufficiently large in the sense that

 $cL > \pi/2.$

For $\sigma \in (0, c)$ define $\omega = \sqrt{c^2 - \sigma^2} > 0$. The pde and f(0) = k g(0) imply

$$f(x) = (c + k\sigma) \sin(\omega x) - k \omega \cos(\omega x),$$

$$g(x) = -(\sigma + kc) \sin(\omega x) - \omega \cos(\omega x).$$

For $k \neq -1$ we have f(L) = g(L) if $\sigma \in (0, c)$ is such that

$$(\sigma + \mathbf{C}) \frac{\tan(\sqrt{\mathbf{C}^2 - \sigma^2} L)}{\sqrt{\mathbf{C}^2 - \sigma^2}} = \frac{k-1}{k+1}.$$

For k = -1 we have f(L) = g(L) if $\sigma \in (0, c)$ is such that

$$\mathbf{0}=\cos(\sqrt{\mathbf{C}^2-\sigma^2}\,\mathbf{L}).$$

This is possible if *c L* is sufficiently large in the sense that

c L
$$> \pi/2$$
 .

With $\sigma = 0$, this is possible if

$$c L = \pi/2.$$
The example by BASTIN and CORON

For $k \neq -1$, in terms of ωL , the condition for non–stabilizability is

$$\left[cL + \sqrt{(cL)^2 - (\omega L)^2}\right] \frac{\tan(\omega L)}{\omega L} = \frac{k-1}{k+1}.$$
(1)

The example by BASTIN and CORON

For $k \neq -1$, in terms of ωL , the condition for non–stabilizability is

$$\left[cL + \sqrt{(cL)^2 - (\omega L)^2}\right] \frac{\tan(\omega L)}{\omega L} = \frac{k-1}{k+1}.$$
(1)

So we analyze the range of the function on the left-hand side of (1)!

We consider

$$F(cL) = \sup_{s \in (0, cL)} \left[cL + \sqrt{(cL)^2 - s^2} \right] \frac{\tan(s)}{s} \ge 0.$$
We substitute $y = cL$. For $y > 0$, define $F(y) = \sup_{s \in (0, y)} \left[y + \sqrt{y^2 - s^2} \right] \frac{\tan(s)}{s}.$

We consider

$$F(cL) = \sup_{s \in (0, cL)} \left[cL + \sqrt{(cL)^2 - s^2} \right] \frac{\tan(s)}{s} \ge 0.$$
We substitute $y = cL$. For $y > 0$, define $F(y) = \sup_{s \in (0, y)} \left[y + \sqrt{y^2 - s^2} \right] \frac{\tan(s)}{s}.$
If $y \ge \pi$, then $F(y) \ge \lim_{s \to \pi^-} \left[\pi + \sqrt{\pi^2 - s^2} \right] \frac{\tan(s)}{s} = 0.$

We consider

$$F(cL) = \sup_{s \in (0, cL)} \left[cL + \sqrt{(cL)^2 - s^2} \right] \frac{\tan(s)}{s} \ge 0.$$
We substitute $y = cL$. For $y > 0$, define $F(y) = \sup_{s \in (0, y)} \left[y + \sqrt{y^2 - s^2} \right] \frac{\tan(s)}{s}.$
If $y \ge \pi$, then $F(y) \ge \lim_{s \to \pi^-} \left[\pi + \sqrt{\pi^2 - s^2} \right] \frac{\tan(s)}{s} = 0.$

For
$$y > 0$$
, define $G(y) = \inf_{s \in (0,y)} \left| y + \sqrt{y^2 - s^2} \right| \frac{\tan(s)}{s}$.

We consider

$$F(cL) = \sup_{s \in (0, cL)} \left[cL + \sqrt{(cL)^2 - s^2} \right] \frac{\tan(s)}{s} \ge 0.$$
We substitute $y = cL$. For $y > 0$, define $F(y) = \sup_{s \in (0, y)} \left[y + \sqrt{y^2 - s^2} \right] \frac{\tan(s)}{s}$

If
$$y \ge \pi$$
, then $F(y) \ge \lim_{s \to \pi^-} \left[\pi + \sqrt{\pi^2 - s^2}\right] \frac{\tan(s)}{s} = 0.$

For
$$y > 0$$
, define $G(y) = \inf_{s \in (0,y)} \left[y + \sqrt{y^2 - s^2} \right] \frac{\tan(s)}{s}$.
If $y > \frac{\pi}{2}$ then $G(y) \le \lim_{s \to \frac{\pi}{2}+} \left[y + \sqrt{y^2 - s^2} \right] \frac{\tan(s)}{s} = -\infty$.
Thus for $y = c L \ge \pi$, the function on the left-hand side of (1) takes all values in $(-\infty, 0]$.

S

We consider

$$F(cL) = \sup_{oldsymbol{s}\in(0,cL)} \left[cL + \sqrt{(cL)^2 - s^2}
ight] \, rac{ an(s)}{s} \geq 0.$$

We substitute y = c L. For y > 0, define $F(y) = \sup_{s \in (0,y)} \left[y + \sqrt{y^2 - s^2} \right] \frac{\tan(s)}{s}$. If $y \ge \pi$, then $F(y) \ge \lim_{s \to \pi^-} \left[\pi + \sqrt{\pi^2 - s^2} \right] \frac{\tan(s)}{s} = 0$.

For
$$y > 0$$
, define $G(y) = \inf_{s \in (0,y)} \left[y + \sqrt{y^2 - s^2} \right] \frac{\tan(s)}{s}$

If
$$y > \frac{\pi}{2}$$
 then $G(y) \leq \lim_{s \to \frac{\pi}{2}+} \left[y + \sqrt{y^2 - s^2} \right] \frac{\tan(s)}{s} = -\infty.$

Thus for $y = c L \ge \pi$, the function on the left-hand side of (1) takes all values in $(-\infty, 0]$.

For all $k \in (-1, 1]$, this implies the instability of the system

because equation (1) has a solution $s = \omega L \in (\pi/2, \pi)$ that corresponds by $\sigma^2 = c^2 - \omega^2$ to $\sigma \in (0, c)$.

Inhalt

Motivation by application: Gas transportation through pipelines Example for a closed-loop system.

The example by BASTIN and CORON: A single interval

A sufficient condition for non-stabilzability A sufficient condition for stabilizability

A tree of strings with a stabilizing and a destabilizing source term Sufficient conditions for non-stabilzability A sufficient condition for stabilizability

The example by BASTIN and CORON

In fact, the following proposition is already proved by BASTIN and CORON:

Proposition:

If $c L \ge \pi$,

there is *no* real value of k such that the closed loop system with the pde

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} + \begin{pmatrix} 0 & c \\ c & 0 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

and the boundary conditions U(t, 0) = k V(t, 0), V(t, L) = U(t, L) is exponentially stable.

The example by BASTIN and CORON

In fact, the following proposition is already proved by BASTIN and CORON:

Proposition:

If $c L \ge \pi$,

there is no real value of k such that the closed loop system with the pde

$$\begin{pmatrix} U \\ V \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix}_{x} + \begin{pmatrix} 0 & c \\ c & 0 \end{pmatrix} \begin{pmatrix} U \\ V \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

and the boundary conditions U(t, 0) = k V(t, 0), V(t, L) = U(t, L) is exponentially stable.

Boundary stabilization becomes **impossible** if the length or the (negative eigenvalue of the) source term is too large!

Inhalt

Motivation by application: Gas transportation through pipelines Example for a closed-loop system.

The example by BASTIN and CORON: A single interval

A sufficient condition for non-stabilzability A sufficient condition for stabilizability

A tree of strings with a stabilizing and a destabilizing source term Sufficient conditions for non-stabilzability A sufficient condition for stabilizability

If $\lambda > 0$, we have $\lambda L < \frac{\pi}{2}$, and for $\epsilon = \frac{\pi}{4} - \frac{\lambda L}{2}$ we have $|k| \le \tan^2(\epsilon)$ and $cL < \lambda \tan^2(\epsilon)$

the system is exponentially stable.

If $\lambda > 0$, we have $\lambda L < \frac{\pi}{2}$, and for $\epsilon = \frac{\pi}{4} - \frac{\lambda L}{2}$ we have $|k| \le \tan^2(\epsilon)$ and $cL < \lambda \tan^2(\epsilon)$

the system is exponentially stable.

This can be seen considering the quadratic LYAPUNOV function

$$\mathcal{L}(t) = \frac{1}{2} \int_0^L A \cot(\epsilon + \lambda x) U^2(t, x) + A^{-1} \tan(\epsilon + \lambda x)) V^2(t, x) dx.$$

If $\lambda > 0$, we have $\lambda L < \frac{\pi}{2}$, and for $\epsilon = \frac{\pi}{4} - \frac{\lambda L}{2}$ we have $|k| \leq \tan^2(\epsilon)$ and $c L < \lambda \tan^2(\epsilon)$

the system is exponentially stable.

This can be seen considering the quadratic LYAPUNOV function

$$\mathcal{L}(t) = \frac{1}{2} \int_0^L A \cot(\epsilon + \lambda x) U^2(t, x) + A^{-1} \tan(\epsilon + \lambda x)) V^2(t, x) dx.$$

 Here the trigonometric weights give a better result (*c L* ≤ 0.177..) than the trigonometric weights.

If $\lambda > 0$, we have $\lambda L < \frac{\pi}{2}$, and for $\epsilon = \frac{\pi}{4} - \frac{\lambda L}{2}$ we have $|k| \le \tan^2(\epsilon)$ and $cL < \lambda \tan^2(\epsilon)$

the system is exponentially stable.

This can be seen considering the quadratic LYAPUNOV function

$$\mathcal{L}(t) = \frac{1}{2} \int_0^L A \cot(\epsilon + \lambda x) U^2(t, x) + A^{-1} \tan(\epsilon + \lambda x)) V^2(t, x) dx.$$

- Here the trigonometric weights give a better result ($c L \le 0.177..$) than the trigonometric weights.
- The choice of the weights is due to the method presented in G. BASTIN, J.-M. CORON, On boundary feedback stabilization of non-uniform linear 2 × 2 hyperbolic systems over a bounded interval, Systems Control Lett. 60 (2011), 900- 906. See also Charlotte's talk!

If $\lambda > 0$, we have $\lambda L < \frac{\pi}{2}$, and for $\epsilon = \frac{\pi}{4} - \frac{\lambda L}{2}$ we have $|k| \le \tan^2(\epsilon)$ and $cL < \lambda \tan^2(\epsilon)$

the system is exponentially stable.

This can be seen considering the quadratic LYAPUNOV function

$$\mathcal{L}(t) = \frac{1}{2} \int_0^L A \cot(\epsilon + \lambda x) U^2(t, x) + A^{-1} \tan(\epsilon + \lambda x)) V^2(t, x) dx.$$

- Here the trigonometric weights give a better result ($c L \le 0.177..$) than the trigonometric weights.
- The choice of the weights is due to the method presented in G. BASTIN, J.-M. CORON, On boundary feedback stabilization of non-uniform linear 2 × 2 hyperbolic systems over a bounded interval, Systems Control Lett. 60 (2011), 900- 906. See also Charlotte's talk!

How is the situation on networks?

Inhalt

Motivation by application: Gas transportation through pipelines Example for a closed-loop system.

The example by BASTIN and CORON: A single interval A sufficient condition for non-stabilzability A sufficient condition for stabilizability

A tree of strings with a stabilizing and a destabilizing source term Sufficient conditions for non-stabilizability A sufficient condition for stabilizability

Now we consider a star-shaped networks of strings.



Figure: A star-shaped network with N = 4 edges.

Now we consider a star-shaped networks of strings.



Figure: A star-shaped network with N = 4 edges.

We consider feedback control at all boundary nodes except one. Let $N \in \{2, 3, 4, ...\}$ denote the number of strings.

Now we consider a star-shaped networks of strings.



Figure: A star-shaped network with N = 4 edges.

We consider feedback control at all boundary nodes except one. Let $N \in \{2, 3, 4, ...\}$ denote the number of strings.

For $i \in \{1, 2, ..., N\}$ let $c_i > 0$ and $\varepsilon_i \ge 0$ be given and consider the wave equation $U_{tt}^i = U_{xx}^i - 2\varepsilon_i U_t^i - (\varepsilon_i^2 - c_i^2) U^i = 0$ (2)

on the space interval $[0, L_i]$.

Now we consider a star-shaped networks of strings.



Figure: A star-shaped network with N = 4 edges.

We consider feedback control at all boundary nodes except one. Let $N \in \{2, 3, 4, ...\}$ denote the number of strings.

For $i \in \{1, 2, ..., N\}$ let $c_i > 0$ and $\varepsilon_i \ge 0$ be given and consider the wave equation $U_{tt}^i = U_{xx}^i - 2\varepsilon_i U_t^i - (\varepsilon_i^2 - c_i^2) U^i = 0$ (2)

on the space interval $[0, L_i]$. The edges are coupled at x = 0 by node conditions:

At the central node:

For *i*, *j* ∈ {1, ..., *N*}

$$U^{i}(t, 0) - U^{j}(t, 0) = 0,$$

 $\sum_{k=1}^{N} U_{x}^{k}(t, 0) = 0.$

At the central node:

For *i*, *j* \in {1, ..., *N*}

$$J^{i}(t, 0) - U^{j}(t, 0) = 0,$$

 $\sum_{k=1}^{N} U_{x}^{k}(t, 0) = 0.$

At the boundary node of edge number 1 at $x = L_1$ we have a homogeneous DIRICHLET condition

 $U_1(t, L_1) = 0$

At the central node:

For *i*, *j* \in {1, ..., *N*}

$$J^{i}(t, 0) - U^{j}(t, 0) = 0,$$

 $\sum_{k=1}^{N} U_{x}^{k}(t, 0) = 0.$

At the boundary node of edge number 1 at $x = L_1$ we have a homogeneous DIRICHLET condition

 $U_1(t, L_1)=0$

and at the other boundary nodes for $j \in \{2, ..., N\}$ at $x = L_j$ we have a NEUMANN velocity feedback

 $U_x^j(t, L_j) = K_j U_t^j(t, L_j)$

with a real *feedback* parameter K_i .

We have a video!

A movie

The wave equation (2) can be transformed to a 2×2 system:

The wave equation (2) can be transformed to a 2 × 2 system: For $i \in \{1, ..., N\}$ define $V^i = -\frac{1}{c_i} (U^i_t + U^i_x + \varepsilon_i U^i)$.

The wave equation (2) can be transformed to a 2 × 2 system: For $i \in \{1, ..., N\}$ define $V^i = -\frac{1}{c_i} (U^i_t + U^i_x + \varepsilon_i U^i)$.

Then due to the definition of V^i and (2), the function (U^i, V^i) solve

$$\begin{pmatrix} U^{i} \\ V^{i} \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U^{i} \\ V^{i} \end{pmatrix}_{x} + \begin{pmatrix} \varepsilon^{i} & c^{i} \\ c_{i} & \varepsilon^{i} \end{pmatrix} \begin{pmatrix} U^{i} \\ V^{i} \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}.$$

The wave equation (2) can be transformed to a 2 × 2 system: For $i \in \{1, ..., N\}$ define $V^i = -\frac{1}{c_i} (U^i_t + U^i_x + \varepsilon_i U^i)$.

Then due to the definition of V^i and (2), the function (U^i, V^i) solve

$$\begin{pmatrix} U^{i} \\ V^{i} \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U^{i} \\ V^{i} \end{pmatrix}_{x} + \begin{pmatrix} \varepsilon^{i} & c^{i} \\ c_{i} & \varepsilon^{i} \end{pmatrix} \begin{pmatrix} U^{i} \\ V^{i} \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}.$$

Also the node conditions and boundary conditions can be transformed similarly:

The wave equation (2) can be transformed to a 2 × 2 system: For $i \in \{1, ..., N\}$ define $V^i = -\frac{1}{c_i} (U^i_t + U^i_x + \varepsilon_i U^i)$.

Then due to the definition of V^i and (2), the function (U^i, V^i) solve

$$\begin{pmatrix} U^{i} \\ V^{i} \end{pmatrix}_{t} + \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix} \begin{pmatrix} U^{i} \\ V^{i} \end{pmatrix}_{x} + \begin{pmatrix} \varepsilon^{i} & c^{i} \\ c_{i} & \varepsilon^{i} \end{pmatrix} \begin{pmatrix} U^{i} \\ V^{i} \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}.$$

Also the node conditions and boundary conditions can be transformed similarly: For example, at $x = L_1$, we have

$$V^{1}(t, L_{1}) = -\frac{1}{c_{1}} \left(U_{x}^{1} + U_{t}^{1} \right)$$

For $i \in \{2, ..., N\}$, at $x = L_i$, we have

$$V^{i}(t, L_{i}) = -rac{1}{c_{i}}\left(arepsilon_{i} U^{i} + (K_{i} + 1) U_{t}^{i}
ight).$$

Aim of this talk

- Also for our star of strings, *boundary feedback stabilization* is *not always possible*!
- If one of the strings is too long, it can become *impossible* for all feedback parameters!

Inhalt

Motivation by application: Gas transportation through pipelines Example for a closed-loop system.

The example by BASTIN and CORON: A single interval A sufficient condition for non-stabilzability A sufficient condition for stabilizability

A tree of strings with a stabilizing and a destabilizing source term Sufficient conditions for non-stabilzability A sufficient condition for stabilizability

Limits of stabilizability: Assume that for all $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i$.

Limits of stabilizability: Assume that for all $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i$.

1. Instability if ALL edges are sufficiently long: If

$$c_1^2 \ge \varepsilon_1^2 + \frac{\pi^2}{L_1^2}$$

and for all $i \in \{2, ..., N\}$ we have

$$c_i = c_1, \ \varepsilon_i = \varepsilon_1, \ L_i = L_1, \ K_i = K_2$$

there are **no values** of $K_2 \in (-\infty, \infty)$ such that the closed loop system with the wave equation (2), the node conditions and the boundary conditions is **asymptotically stable**.

In fact, there are solutions with **exponentially increasing norms** in $X_{i=1}^{N} L^{2}(0, L_{i})$.

Limits of stabilizability: Assume that for all $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i$.

1. Instability if ALL edges are sufficiently long: If

$$c_1^2 \ge \varepsilon_1^2 + \frac{\pi^2}{L_1^2}$$

and for all $i \in \{2, ..., N\}$ we have

$$c_i = c_1, \ \varepsilon_i = \varepsilon_1, \ L_i = L_1, \ K_i = K_2$$

there are **no values** of $K_2 \in (-\infty, \infty)$ such that the closed loop system with the wave equation (2), the node conditions and the boundary conditions is **asymptotically stable**.

In fact, there are solutions with **exponentially increasing norms** in $X_{i=1}^{N} L^{2}(0, L_{i})$.

2. Instability if ONE edge is sufficiently long:

lf

$$C_1^2 > \varepsilon_1^2 + \frac{9}{4} \frac{\pi^2}{L_1^2} \quad \text{and} \quad C_1 - \varepsilon_1 \le \min_{i \in \{2, \dots, N\}} \{C_i - \varepsilon_i\},$$
(3)

there are **no values** of $K_2, ..., K_N \in (-\infty, 0]$ such that the closed loop system is **asymptotically stable**.

Limits of stabilizability: Assume that for $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i = 0$ and one of the values of $L_i > 0$ is sufficiently large.

• Due to the POINCARÉ—inequality, if the $c_i > 0$ are sufficiently small, we can use the energy

$$E(t) = \frac{1}{2} \sum_{i=1}^{N} \int_{0}^{L_{i}} \left(U_{x}^{i}(t, x) \right)^{2} + \left(U_{t}^{i}(t, x) \right)^{2} - c_{i}^{2} \left(U^{i}(t, x) \right)^{2} dx.$$
Limits of stabilizability: Assume that for $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i = 0$ and one of the values of $L_i > 0$ is sufficiently large.

• Due to the POINCARÉ—inequality, if the *c_i* > 0 are sufficiently small, we can use the energy

$$E(t) = \frac{1}{2} \sum_{i=1}^{N} \int_{0}^{L_{i}} \left(U_{x}^{i}(t, x) \right)^{2} + \left(U_{t}^{i}(t, x) \right)^{2} - c_{i}^{2} \left(U^{i}(t, x) \right)^{2} dx.$$

• We have

$$E'(t) = \sum_{i\in I_F} K_i \left(U_t^i(t, L_i)\right)^2.$$

Thus if $K_i \ge 0$, we have $E'(t) \ge 0$ and thus the energy does not decay.

Limits of stabilizability: Assume that for $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i = 0$ and one of the values of $L_i > 0$ is sufficiently large.

• Due to the POINCARÉ—inequality, if the *c_i* > 0 are sufficiently small, we can use the energy

$$E(t) = \frac{1}{2} \sum_{i=1}^{N} \int_{0}^{L_{i}} \left(U_{x}^{i}(t, x) \right)^{2} + \left(U_{t}^{i}(t, x) \right)^{2} - c_{i}^{2} \left(U^{i}(t, x) \right)^{2} dx.$$

• We have

$$E'(t) = \sum_{i\in I_F} K_i \left(U_t^i(t, L_i)\right)^2.$$

Thus if $K_i \ge 0$, we have $E'(t) \ge 0$ and thus the energy does not decay.

 Thus there are no parameter vectors with components K_i ≥ 0 such that the system is asymptotically stable.

Limits of stabilizability: Assume that for $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i = 0$ and one of the values of $L_i > 0$ is sufficiently large.

• Due to the POINCARÉ—inequality, if the c_i > 0 are sufficiently small, we can use the energy

$$E(t) = \frac{1}{2} \sum_{i=1}^{N} \int_{0}^{L_{i}} \left(U_{x}^{i}(t, x) \right)^{2} + \left(U_{t}^{i}(t, x) \right)^{2} - c_{i}^{2} \left(U^{i}(t, x) \right)^{2} dx.$$

• We have

$$E'(t) = \sum_{i\in I_F} K_i \left(U_t^i(t, L_i) \right)^2.$$

Thus if $K_i \ge 0$, we have $E'(t) \ge 0$ and thus the energy does not decay.

- Thus there are no parameter vectors with components K_i ≥ 0 such that the system is asymptotically stable.
- With the Result 2. above, this implies that there are no parameter vectors with components of *equal sign* such that the system is asymptotically stable.

Limits of stabilizability - Result 3.: Instability for a large number of short edges

Assume that for $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i$ and

 $c_i = c_1, \ \varepsilon_i = \varepsilon_1, \ L_i = L_1, \ K_i = K_2.$

Limits of stabilizability - Result 3.: Instability for a large number of short edges

Assume that for $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i$ and

$$c_i = c_1, \ \varepsilon_i = \varepsilon_1, \ L_i = L_1, \ K_i = K_2.$$

lf

$$\sin^2(\sqrt{c_1^2-\varepsilon_1^2}\,L_1)=\frac{1}{N}$$

there are no real values of $K_2 \in (-\infty, \infty)$ ($j \in \{2, ..., N\}$) such that the closed loop system is asymptotically stable.

So here the total length of the strings NL_1^2 must be sufficiently large!

Limits of stabilizability - Result 3.: Instability for a large number of short edges

Assume that for $i \in \{1, ..., N\}$ we have $c_i > \varepsilon_i$ and

$$c_i = c_1, \ \varepsilon_i = \varepsilon_1, \ L_i = L_1, \ K_i = K_2.$$

lf

$$\sin^2(\sqrt{c_1^2-\varepsilon_1^2}\,L_1)=\frac{1}{N}$$

there are no real values of $K_2 \in (-\infty, \infty)$ ($j \in \{2, ..., N\}$) such that the closed loop system is asymptotically stable.

This implies

$$L_1^2 \left(c_1^2 - \varepsilon_1^2 \right) = \left(\arcsin\left(\frac{1}{\sqrt{N}}\right) \right)^2.$$

Since we have $\lim_{N\to\infty} \arcsin(\frac{1}{\sqrt{N}}) = 0$, for *N* sufficiently large we obtain arbitrarily small values of the lengths $L_i > 0$, for which the system is not exponentially stable!

So here the total length of the strings NL_1^2 must be sufficiently large!

Inhalt

Motivation by application: Gas transportation through pipelines Example for a closed-loop system.

The example by BASTIN and CORON: A single interval A sufficient condition for non-stabilzability A sufficient condition for stabilizability

A tree of strings with a stabilizing and a destabilizing source term Sufficient conditions for non-stabilzability A sufficient condition for stabilizability

A sufficient condition for stabilizability

Assume that
$$c_i = c_1$$
, $\varepsilon_i = \varepsilon_1$, $L_i = L_1$, $K_i = K_2$. If $\varepsilon_1 > 0$ and

 $\varepsilon_1 \geq c_1 \geq 0$

with $K_2 = 0$ the closed loop system is exponentially stable.

A sufficient condition for stabilizability

Assume that
$$c_i = c_1$$
, $\varepsilon_i = \varepsilon_1$, $L_i = L_1$, $K_i = K_2$. If $\varepsilon_1 > 0$ and

with $K_2 = 0$ the closed loop system is exponentially stable.

• This can be shown by the analysis of the *eigenfunctions* of the system.

C

 $\leq 01 \leq 0$

• For $\varepsilon_1 \ge c_1 \ge 0$, the matrix of the source term is positive semidefinite.

A sufficient condition for stabilizability

Assume that
$$c_i = c_1$$
, $\varepsilon_i = \varepsilon_1$, $L_i = L_1$, $K_i = K_2$. If $\varepsilon_1 > 0$ and

 $\varepsilon_1 \geq c_1 \geq 0$

with $K_2 = 0$ the closed loop system is exponentially stable.

- This can be shown by the analysis of the *eigenfunctions* of the system.
- For $\varepsilon_1 \ge c_1 \ge 0$, the matrix of the source term is positive semidefinite. What happens for

cL ∈ (0.177.., *π*)?

Thank you for your attention!